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CONTINUOUS METHOD FOR PREPARING ETHYL LACTATE

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The present invention relates to a process for the preparation of ethyl lactate having a purity of greater than 97% starting from lactic acid or from a lactic acid composition.

Ethyl lactate can be used, alone or in combination with other solvents, as cleaning and degreasing agents, in a washing machine and in a nonaqueous medium, for solid surfaces, such as metal components, ceramics, glass or plastics, which have been contaminated by machining oils or greases and/or for their temporary protection.

15 It can also be used for the defluxing of printed circuits, which operation consists in removing the soldering flux.

The methods most widely used industrially for producing ethyl lactate consist of an esterification reaction generally catalyzed by acids, according to the reaction:

 $CH_3CH(OH)CO_2H + E+OH \implies CH_3CH(OH)CO_2CH_2CH_3+ H_2O$ (1)

However, the implementation of this reaction is complicated due to the presence of a hydroxyl group on the lactic acid molecule.

Esterification can thus take place between two lactic acid molecules and can then continue to give lactic acid oligomers, according to the following schemes:

$$2CH_3CH(OH)CO_2H \longrightarrow HOCH(CH_3)CO_2CH(CH_3)CO_2H + H_2O$$
(2)
(II)

II +
$$CH_3CH(OH)CO_2H \implies HOCH(CH_3)CO_2[-CH(CH_3)CO_2]_2H + H_2O$$
 (3)
(III)

$$(II) \xrightarrow{O} CH_3 \cdot H_2O$$

$$(IV)$$

$$nCH_3CH(OH)CO_2H \longrightarrow HOCH(CH_3)CO_2[CH(CH_3)CO_2]_{n-1}H+H_2O$$
 (5)

According to the operating conditions generally used, the lactide (IV) is not formed. On the other hand, the oligomers (II), (III) and/or (V) have been detected for the good reason that, industrially, commercial lactic acid solutions are used.

The term "lactic acid composition" is understood now to 10 mean any aqueous lactic acid solution, whatever its process of preparation and its characteristics, said solution having a highly variable lactic acid purity.

Commercially available solutions comprising 50, 80, 87 or 90% of organic compounds may in particular be concerned, it being understood that such solutions are in fact mixtures of water, of monomers, of dimers and of higher oligomers of lactic acid.

- 20 Thus, in order to productively manufacture ethyl lactate (I), it is necessary not only to esterify the lactic acid monomer but also to depolycondense the oligomers of lactic acid.
- Otherwise, oligomers of ethyl lactate are obtained by esterification of the oligomers of lactic acid, according to the reaction:

$$CH_3CH(OH)CO_2[CH(CH_3)CO_2]_n H + C_2H_5OH \longrightarrow CH_3CH(OH)CO_2[CH(CH_3)C(O)]_nOC_2H_5 + H_2O$$
 (6)

Consequently, in order to minimize, indeed even 30 eliminate, the formation of the oligomers of ethyl

lactate originating from the reaction (6), it is necessary to use a large excess of ethanol and use is generally made of an ethanol/lactic acid molar ratio at least equal to 2.5.

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Furthermore, it should be noted that, during the purification of the crude ethyl lactate obtained by esterification of lactic acid with ethanol, a transesterification reaction between two ethyl lactate molecules can occur, according to the reaction:

$2CH_3CH(OH)CO_2CH_2CH_3 \xrightarrow{CATALYST} > CH_3CH(OH)CO_2CH(CH_3)CO_2CH_2CH_3 + CH_3CH_2OH$ (7)

This transesterification reaction (7) is generally carried out in the presence of basic catalysts, of alkyl orthotitanates or of zirconium-based complexes.

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However, it can also take place by heating during the purification of the ethyl lactate and, in order to prevent it, the purification is generally carried out under reduced pressure.

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Thus, the esterification of lactic acid to give ethyl lactate is rendered more complicated by:

- the presence of oligomers of lactic acid in the starting lactic acid compositions, which it is a matter of depolycondensing in order to obtain the lactic acid,
- the competition between the expected esterification (lactic acid, ethanol) and two esterifications which result in the formation of ethyl lactate oligomer (one esterification between lactic acid and ethyl lactate, another between ethanol and an oligomer of lactic acid).

In addition, the Applicant Company has found that it is possible to form a water/ethyl lactate binary azeotrope, thus complicating the removal of the water from the ethyl lactate.

It is therefore necessary to produce, during the esterification of lactic acid by ethanol, an ethyl lactate having a water content which is as low as possible in order to subject it to a purification consisting of a distillation under reduced pressure.

Consequently, in order to remove the water formed according to the main reaction (1) and optionally according to the reactions (2) and (3) of the esterification reaction medium comprising a mixture of lactic acid, of ethanol, of ethyl lactate, of water and of oligomers, the simplest method is to use the water/ethanol azeotrope.

- However, this results in an ethanol/water mixture which cannot be directly recycled in the reaction medium and, consequently, results in an esterification process which is not very economic industrially.
- 20 To achieve this, it is therefore necessary to carry out the separation of the water from the ethanol by a technique other than distillation.
- In United States patent 5 723 639, the water is selectively removed from the reaction medium by conveying it through a pervaporation membrane.

However, it is expensive to operate in this way, this operation using a technology not employed to any great extent in the basic chemical industry.

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The Applicant Company has found that, in a process for the preparation of ethyl lactate by esterification of lactic acid or of a lactic acid composition (as defined above), it is possible to easily and economically remove the water from the esterification reaction medium.

The present invention thus relates to a continuous

process for the preparation of ethyl lactate (I) by esterification of lactic acid [or of a lactic acid composition] using ethanol, according to the reaction (1):

$$CH_3CH(OH)CO_7H \cdot CH_3CH_2OH = CH_3CH(OH)CO_2CH_2CH_3 \cdot H_2O$$
 (1) (1)

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which consists in reacting said lactic acid with ethanol according to an ethanol/lactic acid initial molar ratio at least equal to 2.5 and preferably ranging from 3 to 4, in the presence of a catalyst, at the reaction medium, 10 reflux of which approximately 100°C, and under an absolute pressure ranging from 1.5 to 3 bar and preferably ranging from 1.5 to 1.8 bar; said process being characterized in that a water/ethanol gas mixture close to the azeotrope 15 is continuously extracted from the esterification reaction medium, in that this gas mixture is then dehydrated directly using molecular sieves, in that an ethanol gas stream, which can be recycled to the esterification reaction medium, and a stream composed of water and of ethanol are then recovered from said 20 dehydration, which stream composed of water and of ethanol is subjected to a distillation, from which water and a water/ethanol azeotrope are obtained, which water/ethanol azeotrope is injected at the top of the 25 for the distillation of the qas extracted from the esterification reaction medium, and in that crude ethyl lactate is then continuously extracted, which crude ethyl lactate is subjected to purification by fractional distillation under reduced pressure, from which an ethyl lactate of high purity 30 and heavy products, which can optionally be recycled to the esterification reaction medium, are obtained.

According to the present invention, the dehydration of 35 the gas mixture extracted from the reaction medium is carried out using the PSA (Pressure Swing Adsorption) technique, which consists in carrying out the selective adsorption of water by passing, at a pressure identical to that applied to the esterification reaction medium, the water/ethanol mixture close to the azeotrope in the gas form through a bed of molecular sieve (adsorption stage) and in then desorbing the water, adsorbed beforehand, by lowering the pressure below 300 mbar and preferably below 100 mbar (desorption stage).

These two stages are carried out alternately.

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According to the present invention, the anhydrous recovered in the adsorption stage advantageously recycled in the esterification reaction while the water-rich phase is subjected to distillation in order to recover pure water and a 15 water/ethanol azeotrope, which is injected at the top of the column for the distillation of the water/ethanol gas mixture extracted from the reaction medium, thus providing reflux in said column, which is not equipped with a condenser. 20

The reaction is advantageously carried out in the presence of an acid catalyst which is soluble or insoluble in the esterification reaction medium.

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Mention will be made, as examples of soluble catalysts which can be used according to the present invention, of 98% H_2SO_4 , H_3PO_4 or methanesulfonic acid.

30 Preferably, 98% H_2SO_4 will be used.

The catalyst according to the invention is used at molar contents ranging from 0.1% to 4% and preferably at contents ranging from 0.2% to 3%, with respect to the 100% lactic acid employed.

According to the present invention, it is possible to operate in a stirred reactor or using a "fixed bed" technology. In the latter case, solid catalysts, such

as ion-exchange resins of the Amberlyst 15 type, will be used.

The initial or start-up time for the esterification can vary to a large extent. It is generally at most equal to 12 hours and preferably between 5 and 12 hours.

The stream of the products exiting from esterification reaction medium, comprising predominantly ethyl lactate and ethanol, along with 10 traces of water and of heavy products (oligomers), is to fractional distillation under reduced pressure according to the techniques normal to a person skilled in the art.

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An ethyl lactate with a purity at least equal to 99% is obtained as top product, and heavy products, which can be recycled in the esterification reaction medium, are obtained as distillation bottom product.

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The process according to the present invention can be carried out in a device as represented in figure 1.

This device comprises:

- 25 a reactor (1), optionally provided with a stirrer, equipped with temperature probes, with a feed for lactic acid (2), with a feed for ethanol (3) and with a feed for catalyst (4);
- a distillation column (5), devoid of condenser,
 30 having between 5 and 15 theoretical plates, fed
 with gas phase extracted from the reactor (1) via
 the feed (6);
- a PSA device (7) composed of 2 identical columns (A and B) filled with molecular sieve which operate alternately in adsorption and in desorption; said PSA device, fed with gas phase from the distillation column (5) via the feed (8), is equipped with an outlet (9) connected to the column operating in adsorption which makes it

possible to feed the esterification reactor with ethanol (gas) and with an outlet (10) connected to the column operating in desorption which makes it possible to feed a distillation column (11) with water/ethanol mixture; said distillation column (11) is equipped with an outlet (12) for discharging the water and with an outlet (13) for conveying the water/ethanol azeotrope to the top of the distillation column (5);

on outlet for the esterification products (14) feeding a purification region (15) from which the ethanol with water exits via (16), the pure ethyl lactate exits via (17) and heavy products exit via (18), which heavy products can be recycled to the esterification reactor after a bleed at (19).

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The process according to the present invention applies very particularly to the esterification by ethanol of the lactic acid present in commercial lactic acid compositions as defined above.

Preferably, use will be made of lactic acid compositions comprising 87% by weight of lactic acid.

- The process according to the present invention makes it possible to completely convert the lactic acid of said compositions and to depolymerize the oligomers present in said lactic acid compositions used.
- 30 The ethyl lactate originating from the esterification reactor does not comprise much water, which makes it possible to easily purify it.

To operate in the way according to the present invention also makes possible the extraction from the reaction medium of a gas phase virtually devoid of the ethyl lactate formed.

The example which follows illustrates the invention.

EXAMPLE

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- Preparation of ethyl lactate

A test is carried out in a device as represented in figure 1.

The reactor (1) has a capacity of 2 1.

The PSA system (7) is composed of 2 identical columns (A and B) filled with molecular sieves, Siliporite NK30, 3 Å.

The distillation column is filled with a Sulzer Ex packing with a diameter equal to 20 mm. It has 10 theoretical plates.

The course of the test was as follows:

- 15 In a first step, a lactic acid composition is esterified with ethanol under batchwise conditions in the reactor (1). The esterification is carried out at a pressure greater than atmospheric pressure and at a temperature in the region of 100°C.
 - when the Then, in a second step, degree the lactic acid has conversion of approximately 95%, the esterification reaction is continued continuously in accordance with the invention according present to operating conditions described below.
 - <u>Batchwise esterification</u> (start-up)

 The following are introduced into the reactor (1):
- 30 391 g of an 87% lactic acid composition, i.e. 342 g of 100% lactic acid (3.8 mol),
 - 667.4 g of absolute ethanol, i.e. 14.5 mol, which corresponds to an ethanol/lactic acid initial molar ratio equal to 3.81,
- 35 3.3 g of 98% $\rm H_2SO_4$ (0.033 mol), i.e. 0.86 mol% with respect to the lactic acid employed.

The reactor is placed under a pressure of 1.5 bar and then the reaction medium is stirred and brought to

reflux, which corresponds to a temperature substantially equal to 100°C.

In order to bring the batch to complete conversion (greater than 95%), a gas mixture comprising water and ethanol is continuously extracted from the reaction medium using the distillation column (5), at a column bottom temperature in the region of 100°C and absolute pressure equal to 1.5 bar, and then this mixture is dehydrated by conveying it into the PSA 10 system (7) which operates under an absolute pressure of 1.5 bar, from which pure ethanol exits at (9), which ethanol continuously feeds the esterification reaction medium present in the reactor, and from which a water/ ethanol mixture exits at (10) during the desorption 15 stage, which water/ethanol mixture is distilled in the distillation column (11), from which a water/ethanol azeotrope exits at (13), which water/ethanol azeotrope is directed to the top of the distillation column (5), thus making it possible to provide reflux at the top of 20 said distillation column. The water exits at (12).

The progress of the reaction is monitored by determining the degree of conversion of the lactic 25 acid, measured by GC.

When the degree of conversion of the lactic acid has reached approximately 95%, which is achieved approximately at the end of 6 hours, the esterification is continued continuously.

The PSA operates in an identical fashion throughout the manufacturing operation.

35 - Continuous esterification

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Then, simultaneously, the esterification reaction medium is fed continuously with:

- 87% lactic acid composition,
- fresh ethanol plus ethanol recycled via (9), while

maintaining the fresh ethanol/lactic acid molar ratio in the region of 4,

- 98% sulfuric acid and heavy products originating from the purification region (15) via (18).

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Simultaneously, a mixture comprising ethyl lactate, ethanol, H_2SO_4 and traces of water exits via the pipe (14), said crude ethyl lactate being purified by distillation under reduced pressure in the purification region (15).

When the system is operating under stationary conditions, on the one hand the esterification is monitored by analyzing the degree of conversion and the yield of the esterification (by GC) and, on the other hand, the distillation is monitored by analyzing the binary mixture collected as top product from the column (5), which operates with a reflux ratio in the region of 0.27. The residence time is 6 hours.

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After the reactor has been replenished 4 times, i.e. operating for 30 hours (including the reaction time under batchwise conditions), a gas mixture having the following composition by weight (mean):

- 25 3.9% of water,
 - 96.1% of ethanol,

is present at the outlet of the column (5) and a mixture having the following composition by weight (mean):

- 30 2.2% of water,
 - 66.3% of ethanol,
 - 27.6% of ethyl lactate,
 - 1.3% of dimer of ethyl lactate,

is present at the outlet of the reactor (14).